

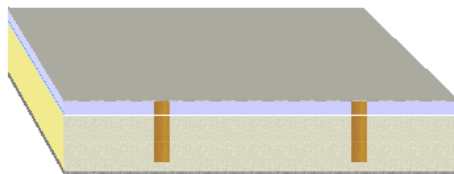
Documentation of the component
 Thermal transmittance (U-value) according to BS EN ISO 6946

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 Source: **own catalogue**
 Component: **New roof**

OUTSIDE

This illustration of inhomogeneous layers is provided only to assist in visualising the arrangement.



On the basis of the given information about the inhomogeneous layers, it is not possible to estimate how and where bearing elements intersect each other. It was assumed that the layers intersect crosswise. The size of the areas was calculated corresponding to their percentage of the whole area.

INSIDE

 Assignment: Roof with a pitch $\geq 70^\circ$

	Manufacturer	Name	Thickness [m], number	Lambda [W/(mK)]	Q	R [m ² K/W]
<input type="checkbox"/>	Rse					0.1300
<input type="checkbox"/>	1 BS EN 12524	Slate [2000 kg/m ³]	0.0050	2.200	D	0.0023
<input type="checkbox"/>	2	Inhomogeneous material layer	0.0500	∅ 0.010		4.8077
	2a BS EN ISO 6946	Well ventilated air layer	92.00 %	0.000	D	-
	2b BS EN 12524	Softwood Timber [500 kg/m ³]	08.00 %	0.130	D	-
<input checked="" type="checkbox"/>	3 BS EN 12524	Breather membrane	0.0001	0.170	D	0.0006
<input checked="" type="checkbox"/>	4	Inhomogeneous material layer	0.1750	∅ 0.035		4.9659
	4a Synthesia	Synthesia 303 HFO	92.00 %	0.027	E	-
	Air gaps	Level 1: dU" = 0.01 W/(m ² K)				
	4b Generic Building Materials	Softwood Timber [500 kg/m ³]	08.00 %	0.130	D	-
<input checked="" type="checkbox"/>	5 Xtratherm Limited	Thin-R XT/PR Pitched Roof	0.0400	0.022	C	1.8182
	Air gaps	Level 1: dU" = 0.01 W/(m ² K)				
<input checked="" type="checkbox"/>	6 BS EN 12524	Gypsum plasterboard	0.0125	0.250	D	0.0500
	Rsi					0.1300
			0.2826			

 was not taken into consideration in the calculation

$$R_T = (R_T' + R_T'')/2 = 7.40 \text{ m}^2\text{K/W}$$

Correction to U-value for	according to	delta U [W/(m ² K)]
Air gaps	BS EN ISO 6946 Annex D	0.005
		0.005

$$U = 1/R_T + \Sigma \Delta U = 0.14 \text{ W/(m}^2\text{K)}$$

- Q .. The physical values of the building materials has been graded by their level of quality. These 5 levels are the following
- A** .. A: Data is entered and validated by the manufacturer or supplier. Data is continuously tested by 3rd party.
 - B** .. B: Data is entered and validated by the manufacturer or supplier. Data is certified by 3rd party
 - C** .. C: Data is entered and validated by the manufacturer or supplier.
 - D** .. D: Information is entered by BuildDesk without special agreement with the manufacturer, supplier or others.
 - E** .. E: Information is entered by the user of the BuildDesk software without special agreement with the manufacturer, supplier or others.

$$U_{\max} = \boxed{0.20 \text{ W/(m}^2\text{K)}}$$

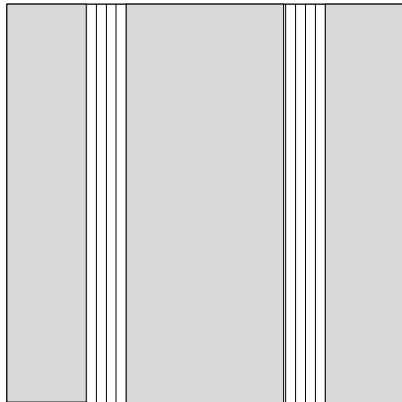
$$U = \boxed{0.14 \text{ W/(m}^2\text{K)}} \quad R_T = \boxed{7.40 \text{ m}^2\text{K/W}}$$

Source of Umax value: England and Wales Approved Document L1A 2010 Tab 2 Dwellings New



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Draft of the component (portion in %):
 23.00 4.00 46.00 4.00 23.00



The inhomogeneous layer consists of two zones (A, B).
 The portion is given in %.

A	 23.00 + 46.00 + 23.00 consisting of material layers: 3, 4a, 5, 6	= 92.00%
B	 4.00 + 4.00 consisting of material layers: 3, 4b, 5, 6	= 8.00%

Upper limit of the thermal transfer resistance R

$$U_A \text{ [W/(m}^2\text{K)]} = \frac{1}{(\sum R_{i,A}) + R_{si} + R_{se}} = \frac{1}{8.35 + 0.13 + 0.13} = 0.12$$

$$U_B \text{ [W/(m}^2\text{K)]} = \frac{1}{(\sum R_{i,B}) + R_{si} + R_{se}} = \frac{1}{3.21 + 0.13 + 0.13} = 0.29$$

$$R_T' = \frac{1}{A * U_A + B * U_B} = 7.70 \text{ m}^2\text{K/W}$$

Lower limit of the thermal transfer resistance R

R_{se} [m ² K/W]		= 0.13
R_3'' [m ² K/W] = $d_3 / \lambda_3 =$	0.0001 / 0.170	= 0.00
R_4'' [m ² K/W] = $d_4 / (\lambda_{4a} * A + \lambda_{4b} * B) =$	0.1750 / (0.027 * 92.00% + 0.130 * 8.00%)	= 4.97
R_5'' [m ² K/W] = $d_5 / \lambda_5 =$	0.0400 / 0.022	= 1.82
R_6'' [m ² K/W] = $d_6 / \lambda_6 =$	0.0125 / 0.250	= 0.05
R_{si} [m ² K/W]		= 0.13

$$R_T'' = \sum R_i'' + R_{si} + R_{se} = 7.09 \text{ m}^2\text{K/W}$$